

This Page Is Inserted by IFW Operations
and is not a part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

IMAGES ARE BEST AVAILABLE COPY.

**As rescanning documents *will not* correct images,
please do not report the images to the
Image Problem Mailbox.**

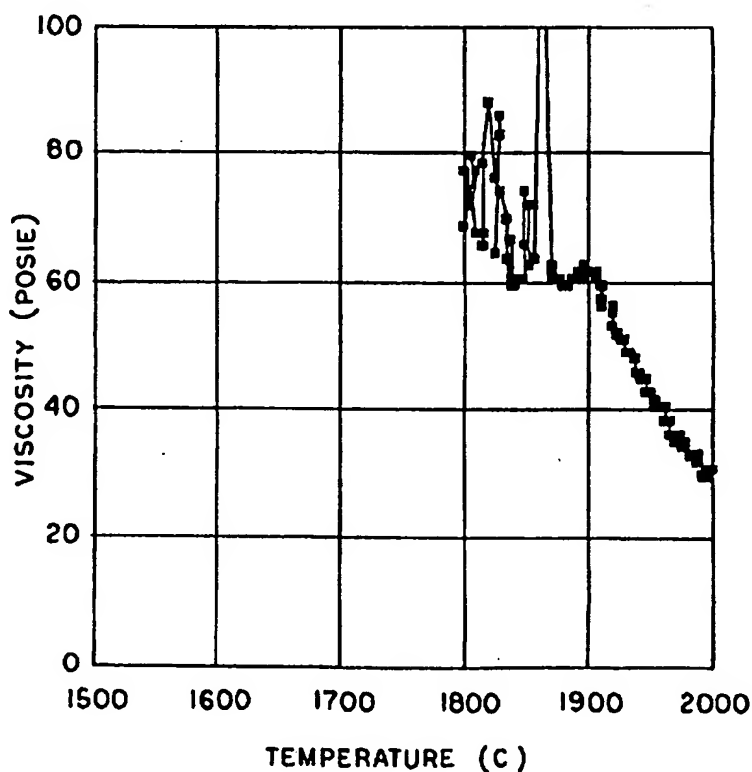
PCTWORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau

INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶: C03C 13/02	A1	(11) International Publication Number: WO 97/16386 (43) International Publication Date: 9 May 1997 (09.05.97)
(21) International Application Number: PCT/US96/17494 (22) International Filing Date: 29 October 1996 (29.10.96) (30) Priority Data: 60/008,064 : 30 October 1995 (30.10.95) US (71) Applicant: UNIFRAX CORPORATION [US/US]; 2351 Whirlpool Street, Niagra Falls, NY 14305 (US). (72) Inventors: ZOITOS, Bruce, K.; 947 Delaware Avenue, Buffalo, NY 14209 (US). ATKINSON, Richard, E., A.; 51460 Outer Drive, South Bend, IN 46628 (US). OLSON, James, R.; 485 Northfield Drive, Youngstown, NY 44174 (US). (74) Agents: CURATOLO, Joseph, G. et al.; Renner, Kenner, Greive, Bobak, Taylor and Weber, 16th floor, First National Tower, Akron, OH 44308-1456 (US).		(81) Designated States: AU, BR, CA, CN, JP, KR, MX, SG, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>

(54) Title: HIGH TEMPERATURE RESISTANT GLASS FIBER**(57) Abstract**

A refractory glass fiber having a use temperature of greater than 1000 °C, up to at least 1260 °C, having an after service mechanical integrity comparable to conventional refractory ceramic fiber and which is non-durable in physiological fluids, consisting essentially of the product of silica, magnesia and optionally zirconia, is produced from a melt, optionally containing a viscosity modifier.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AM	Armenia	GB	United Kingdom	MW	Malawi
AT	Austria	GE	Georgia	MX	Mexico
AU	Australia	GN	Guinea	NE	Niger
BB	Barbados	GR	Greece	NL	Netherlands
BE	Belgium	HU	Hungary	NO	Norway
BF	Burkina Faso	IE	Ireland	NZ	New Zealand
BG	Bulgaria	IT	Italy	PL	Poland
BJ	Benin	JP	Japan	PT	Portugal
BR	Brazil	KE	Kenya	RO	Romania
BY	Belarus	KG	Kyrgyzstan	RU	Russian Federation
CA	Canada	KP	Democratic People's Republic of Korea	SD	Sudan
CF	Central African Republic	KR	Republic of Korea	SE	Sweden
CG	Congo	KZ	Kazakhstan	SG	Singapore
CH	Switzerland	LI	Liechtenstein	SI	Slovenia
CI	Côte d'Ivoire	LK	Sri Lanka	SK	Slovakia
CM	Cameroon	LR	Liberia	SN	Senegal
CN	China	LT	Lithuania	SZ	Swaziland
CS	Czechoslovakia	LU	Luxembourg	TD	Chad
CZ	Czech Republic	LV	Latvia	TG	Togo
DE	Germany	MC	Monaco	TJ	Tajikistan
DK	Denmark	MD	Republic of Moldova	TT	Trinidad and Tobago
EE	Estonia	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	UG	Uganda
FI	Finland	MN	Mongolia	US	United States of America
FR	France	MR	Mauritania	UZ	Uzbekistan
GA	Gabon			VN	Viet Nam

HIGH TEMPERATURE RESISTANT GLASS FIBER

5

TECHNICAL FIELD

The present invention is directed to high temperature resistant glass fiber, useful as a heat or sound insulating material, which has a use temperature limit at least up to 1260°C. More particularly, the present invention is directed to high temperature resistant fiber that is easily manufacturable, and which exhibits low shrinkage and retains good mechanical strength after exposure to the service temperature, yet which is non-durable in physiological fluids.

20

BACKGROUND OF THE INVENTION

The insulation material industry has determined that it is desirable to utilize fibers in heat and sound insulating applications which are not durable in physiological fluids, such as lung fluid. While candidate materials have been proposed, the use temperature limit of these materials have not been high enough to accommodate many of the applications to which high temperature resistant fibers, including refractory glass and ceramic fibers, are applied. In particular, high temperature resistant fibers should exhibit minimal linear shrinkage at expected exposure temperatures, in order to provide effective thermal protection to the article being insulated.

35

Many compositions within the man-made vitreous fiber family of materials have been proposed which are decomposable in a physiological medium. These glass fibers generally have a significant alkali metal oxide content,
5 which often results in a low use temperature limit.

Canadian Patent Application 2017344 describes a glass fiber having physiological solubility formed from glasses containing as required components silica, calcia and Na_2O ,
10 as preferred components, magnesia and K_2O , and as optional components boria, alumina, titania, iron oxides, and fluoride.

International Publication WO 90/02713 describes
15 mineral fibers which are soluble in saline solutions, the fibers having a composition including silica, alumina, iron oxide, calcia, magnesia, Na_2O and K_2O .

U.S. Patent 5,108,957 describes glass compositions
20 useful for forming fibers which are able to be degraded in a physiological medium containing as required components silica, calcia, Na_2O plus K_2O , and boria, and optionally alumina, magnesia, fluoride and P_2O_5 . It describes the presence of phosphorus as having the effect of increasing
25 the rate of decomposition of the fibers in a physiological medium.

Other patents which cite the effect of phosphorus in favoring biological solubility of mineral fibers include
30 International Publication WO 92/09536, describing mineral fibers containing substantially silica and calcia, but optionally magnesia and Na_2O plus K_2O , in which the presence of phosphorus oxide decreases the stabilizing effect of aluminum and iron on the glass matrix. These fibers are
35 typically produced at lower temperatures than refractory ceramic fibers. We have observed that at melt temperatures

required for high temperature resistant fibers (1700-2000°C), phosphorus oxide at levels as low as a few percent can cause severe degradation and/or erosion of furnace components.

5

Canadian Patent Application 2043699 describes fibers which decompose in the presence of a physiological medium, which contain silica, alumina, calcia, magnesia, P_2O_5 , optionally iron oxide, and Na_2O plus K_2O . French Patent Application 2662687 describe mineral fibers which decompose in the presence of a physiological medium, which contain silica, alumina, calcia, magnesia, P_2O_5 , iron oxide and Na_2O plus K_2O plus TiO_2 .

15

U.S. Patent 4,604,097 describes a bioabsorbable glass fiber comprising generally a binary mixture of calcia and phosphorous pentoxide, but having other constituents such as calcium fluoride, water, and one or more oxides such as magnesia, zinc oxide, strontium oxide, sodium oxide, potassium oxide, lithium oxide or aluminum oxide.

20

International Publication WO 92/07801 describes a bioabsorbable glass fiber comprising phosphorous pentoxide, and iron oxide. A portion of the P_2O_5 may be replaced by silica, and a portion of the iron oxide may be replaced by alumina. Optionally the fiber contains a divalent cation compound selected from Ca, Zn and/or Mg, and an alkali metal cation compound selected from Na, K, and/or Li.

25

U.S. Patent 5,055,428 describes a soda lime aluminoboro-silicate glass fiber composition which is soluble in a synthetic lung solution. Alumina content is decreased with an increase in boria, and an adjustment in silica, calcia, magnesia, K_2O and optionally Na_2O . Other components may include iron oxide, titania, fluorine, barium oxide and zinc oxide.

30
35

International Publication WO 87/05007 describes inorganic fiber having solubility in saline solution and including silica, calcia, magnesia, and optionally alumina. International Publication WO 89/12032 describes inorganic fiber having extractable silicon in physiological saline solution and including silica, calcia, optionally magnesia, alkali metal oxides, and one or more of alumina, zirconia, titania, boria and iron oxides.

International Publication WO 93/15028 describes vitreous fibers that are saline soluble which in one usage crystallize to diopside upon exposure to 1000°C and/or 800°C for 24 hours and have the composition described in weight percent of silica 59-64, alumina 0-3.5, calcia 19-23 and magnesia 14-17, and which in another usage crystallize to wollastonite/pseudowollastonite and have the composition described in weight percent of silica 60-67, alumina 0-3.5, calcia 26-35 and magnesia 4-6.

The fibers described in the above identified patent publications are limited, however, in their use temperature, and are therefore unsuitable for high temperature insulation applications, such as furnace linings for use above 1000°C, and reinforcement applications such as metal matrix composites and friction applications.

A product based on non-durable fiber chemistry is marketed by Unifrax Corporation (Niagara Falls, New York) under the trademark INSULFRAX, having the nominal weight percent composition of 65% SiO₂, 31.1% CaO, 3.2% MgO, 0.3% Al₂O₃, and 0.3% Fe₂O₃. Another product is sold by Thermal Ceramics (located in Augusta, Georgia) under the trademark SUPERWOOL, and is composed of 58.5% SiO₂, 35.4% CaO, 4.1% MgO and 0.7% Al₂O₃, by weight. This material has a use limit of 1000°C and melts at approximately 1240°C, which is too

low to be desirable for the high temperature insulation purposes described above.

5 International Application WO 94/15883 discloses
CaO/MgO/SiO₂ fibers with additional constituents Al₂O₃, ZrO₂,
and TiO₂, for which saline solubility and refractoriness
were investigated. That document states that saline
solubility appeared to increase with increasing amounts of
MgO, whereas ZrO₂ and Al₂O₃ were detrimental to solubility.
10 The presence of TiO₂ (0.71-0.74 mol%) and Al₂O₃ (0.51-0.55
mol%) led to the fibers failing the shrinkage criterion of
3.5% or less at 1260°C. The document further states that
fibers that are too high in SiO₂ are difficult or impossible
to form, and cites samples having 70.04, 73.28 and 78.07%
15 SiO₂ as examples which could not be fiberized.

In addition to temperature resistance as expressed by
shrinkage characteristics that are important in fibers that
are used in insulation, it is also required that the fibers
20 have mechanical strength characteristics during and
following exposure to the use or service temperature, that
will permit the fiber to maintain its structural integrity
and insulating characteristics in use.

25 One characteristic of the mechanical integrity of a
fiber is its after service friability. The more friable a
fiber, that is, the more easily it is crushed or crumbled
to a powder, the less mechanical integrity it possesses.
We have observed that, in general, refractory fibers that
30 exhibit both high temperature resistance and non-durability
in physiological fluids also exhibit a high degree of after
service friability. This results in the fiber's lacking
the strength or mechanical integrity after exposure to the
service temperature to be able to provide the necessary
35 structure to accomplish its insulating purpose.

We have found that high temperature resistant, non-durable fibers which do exhibit good mechanical integrity have very small-scale or fine crystalline microstructures after exposure to service temperature. Other measures of mechanical integrity of fibers include compression strength and compression recovery.

Refractory glass compositions which may exhibit target durability, shrinkage at temperature, and strength characteristics may not, however, be susceptible to fiberization, either by spinning or blowing from a melt of its components.

It is therefore an object of the present invention to provide high temperature resistant refractory glass fiber, that is readily manufacturable from a melt having a viscosity suitable for blowing or spinning fiber, and which is non-durable in physiological fluids.

It is a further object of the present invention to provide high temperature resistant refractory glass fiber, which is non-durable in physiological fluids, and which exhibits good mechanical strength after exposure to service temperature.

It is a further object of the present invention to provide high temperature resistant refractory glass fiber, which is non-durable in physiological fluids, yet which exhibits low after service friability.

It is a further object of the present invention to provide high temperature resistant refractory glass fiber, which is non-durable in physiological fluids, and which preferably exhibits a small-scale or fine microstructure after initial exposure to service temperature.

It is a further object of the present invention to provide high temperature resistant refractory glass fiber, which is non-durable in physiological fluids, and which exhibits high compression strength and recovery from compression after exposure to service temperature.

SUMMARY OF THE INVENTION

High temperature resistant refractory glass fibers are provided which are non-durable in physiological fluids. The fibers are 4 to 150 times more soluble in simulated lung fluid than standard aluminosilicate refractory ceramic fibers, and exhibit a temperature use limit of from at least 1000° up to 1260°C, or greater. At these high temperatures, fibers of the present invention as described below undergo less than about a 6% linear shrinkage, preferably less than about a 4.5% linear shrinkage, and most preferably less than about 3% linear shrinkage when held at temperature for 24 or 168 hours. The fibers of the present invention retain mechanical strength after exposure to service temperatures. In contrast to the teachings of the art, fibers of the present invention meeting the requirements of being fiberizable, refractory, and non-durable, have been identified in which the compositions contain SiO₂ in the range of 70 to 86 weight percent.

According to the present invention, there is provided a low shrinkage, refractory glass fiber based on a magnesium silicate system having a use temperature up to at least 1260°C, which maintains mechanical integrity after exposure to the use temperature and which is non-durable in physiological fluids, such as lung fluid.

The non-durable refractory glass fiber according to one embodiment of the present invention consists essentially of the product of about 65 to about 86 weight

percent silica, about 14 to about 35 weight percent
magnesia, 0 to about 11 weight percent zirconia and,
optionally, an effective amount of a viscosity modifier.
The viscosity modifier may be selected from alumina, boria
5 and mixtures thereof. The fiber should contain not more
than about 1 weight percent calcia impurity and not more
than about 0.4 weight percent iron oxides impurity,
(calculated as Fe_2O_3).

10 The fibers of the present invention preferably contain
substantially no alkali metal, greater than trace
impurities. The presence of iron oxides and calcia should
be limited to the extent possible.

15 The present invention provides a process for the
production of refractory glass fiber having a use
temperature up to at least 1260°C , which maintains
mechanical integrity after exposure to the service
temperature and which is non-durable in physiological
20 fluids comprising:

forming a melt with the ingredients consisting
essentially of about 65 to about 86 weight percent silica,
about 14 to about 35 weight percent magnesia, 0 to about 11
weight percent zirconia and, optionally, an effective
25 amount of a viscosity modifier, and
producing fibers from the melt.

The melt compositions utilized to produce the fibers
of the present invention provide a melt viscosity suitable
30 for blowing or spinning fiber, and for controlling crystal
structure of the resultant fibers so as to impart
mechanical strength after exposure to service temperature.

35 BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1A is a viscosity vs. temperature curve of a

melt chemistry for a commercially available, spun aluminosilicate fiber.

5 Figure 1B is a viscosity vs. temperature curve of a melt chemistry for a commercially available, blown aluminosilicate fiber.

10 Figure 2 is a viscosity vs. temperature curve for a magnesia-silica-zirconia fiber melt chemistry having 75% by weight silica.

15 Figure 3 is a viscosity vs. temperature curve for a magnesia-silica-zirconia fiber melt chemistry having 70% by weight silica.

 Figure 4 is a viscosity vs. temperature curve for a magnesia-silica-zirconia fiber melt chemistry having 75% by weight silica and 1 weight percent added alumina.

20 Figure 5 is a viscosity vs. temperature curve for a preferred magnesia-silica-zirconia fiber melt chemistry having 1 weight percent added alumina.

25 Figure 6 is a viscosity vs. temperature curve for a preferred magnesia-silica-zirconia fiber melt chemistry.

 Figure 7 is a viscosity vs. temperature curve for a preferred magnesia-silica-zirconia fiber melt chemistry.

30 Figure 8 is a scanning electron micrograph of ceramic fibers comprising aluminum zirconium silicate (AZS) following exposure to 1426°C for 24 hours.

35 Figure 9 is a scanning electron micrograph of ceramic fibers comprising kaolin following exposure to 1260°C for 24 hours.

Figure 10 is a scanning electron micrograph of glass fibers comprising titanium calcium silicate following exposure to 1260°C for 24 hours.

5 Figure 11 is a scanning electron micrograph of glass fibers of the present invention following exposure to 1260°C for 24 hours.

10 Figure 12 is a scanning electron micrograph of a cross section of glass fibers of the present invention.

15 Figure 13 is a scanning electron micrograph of a cross section of ceramic fibers comprising aluminum zirconium silicate (AZS).

DETAILED DESCRIPTION OF THE INVENTION

20 According to the present invention, there is provided refractory glass fiber useful as a heat or sound insulation material, which has a temperature use limit greater than 1260°C and which is non-durable in physiological fluids, such as lung fluid. By non-durable in physiological fluids is meant that the fiber at least partially dissolves in
25 such fluids (such as simulated lung fluid) during in vitro tests.

30 In order for a glass composition to be a viable candidate for producing a satisfactory high temperature refractory fiber product, the fiber to be produced must be manufacturable, sufficiently soluble in physiological fluids, and capable of surviving high temperatures with minimal shrinkage and minimal loss of integrity. To
35 identify materials which meet these criteria, a set of screening tests were used to identify fibers that exhibit the target properties. These tests include (a) viscosity/fiberization, (b) durability, (c) shrinkage at

temperature and (d) after-service friability, strength and resilience.

5 "Viscosity" refers to the ability of a glass melt to resist flow or shear stress. The viscosity-temperature relationship is critical in determining whether it is possible to fiberize a given glass composition. An optimum viscosity curve would have a low viscosity (5-50 poise) at the fiberization temperature and would gradually increase as the temperature decreased. If the melt is not sufficiently viscous (ie. too thin) at the fiberization temperature, the result is a short, thin fiber, with a high proportion of unfiberized material (shot). If the melt is too viscous at the fiberization temperature, the resulting fiber will be extremely coarse (high diameter) and short.

20 Viscosity is dependent upon melt chemistry, which is also affected by elements or compounds that act as viscosity modifiers. We have found for this fiber chemistry system, that alumina and boria act as viscosity modifiers which permit fibers to be blown or spun. It is necessary, however, according to the present invention, that such viscosity modifiers, either by type or amount, do not adversely impact the solubility, shrink resistance, or mechanical strength of the blown or spun fiber.

30 Viscosity-temperature profiles may be measured on a viscometer, capable of operating at elevated temperatures. In addition, an adequate viscosity profile may be inferred by routine experimentation, examining the quality of fiber (index, diameter, length) produced.

35 The durability test measures the rate at which mass is lost from the fiber ($\text{ng}/\text{cm}^2\text{-hr}$) under conditions which simulate the temperature and chemical conditions found in the human lung. This test consists of exposing

approximately 0.1g of de-shotted fiber to a 0.3 ml/min flow of simulated lung fluid (SLF). The entire test system is maintained at 37°C, to simulate the temperature of the human body. Tests preferably last for between about two and four weeks.

After the SLF has flowed through the fiber, it is collected and analyzed for glass constituents using Inductively Coupled Plasma Spectroscopy. A "blank" SLF sample is also measured and used to correct for elements present in the SLF. Once this data has been obtained, it is possible to calculate the rate at which the fiber has lost mass over the time interval of the study.

Fibers are tested for shrinkage by wet-forming them into a pad, measuring by means of calipers the pad's length and width dimensions (typically 3 x 5 inches), placing the pad into a furnace, ramping to temperature and holding for a fixed period of time. After heating, the pads are re-measured to determine any changes in dimension which have occurred.

In one such test, pads were made by mixing about 427 grams fiber, 27.2 grams of phenolic binder and about 4 gallons of water, pouring the mixture into a sheet mold and allowing the water to drain through the bottom of the mold. The pad was dried and a piece measuring 3 inches by 5 inches by 1 inch was cut. The length and width of this piece were carefully measured, and the pad was placed in a furnace and brought to a temperature of 1260°C for 24, 168 or 672 hours. After cooling, the lateral dimensions were measured and the linear shrinkage was determined by comparing "before" and "after" measurements. If the fiber is available in blanket form, measurements may be made directly on the blanket without the need to form a pad. (Such blanket shrinkage measurements correlate to, but are

not identical to, pad shrinkage measurements.)

After-service friability refers to the ability of fiber to retain its mechanical integrity after exposure to high temperatures. This is an important property, since fiber must support its own weight in any application and must also be able to resist abrasion due to moving air or gas. Indications of fiber integrity and mechanical strength are provided by visual and tactile observations, as well as mechanical measurement of these properties of after-service temperature exposed fibers.

Shrinkage pad after service integrity is indicated by two tests: compression strength and compression recovery. These tests measure, respectively, how easily the pad may be deformed and the amount of resiliency (or compression recovery) the pad exhibits after a compression of 50%.

Shrinkage pads prepared from fibers of the present invention were heated at 1260°C for 24 or 168 hours, and were then compression tested using an Instron testing device. A 2.5 inch diameter cylindrical ram was pushed into the shrinkage pad until the pad was compressed to half its original thickness. At this point, the crosshead was stopped and the peak load (in psi) encountered during compression was recorded.

Compression recovery was then measured by slowly reversing the travel direction of the crosshead and backing the cylindrical ram out of the shrinkage pad until the load reading was zero. The distance of travel from the 50% compression point to the zero load point was recorded and expressed as a percentage of original pad thickness. This number is indicative of the amount of resiliency of the fiber pad.

By this testing criteria, a poorly performing pad would have low values for compressive strength indicating that it is easily compressed, and low values for compression recovery indicating that once deformed the pad experiences little recovery. Conversely, a pad/fiber composition with high values for these parameters exhibits high mechanical strength and is considered a good-performer. An ideal fiber would have a compressive strength within a target range comparable to a standard, commercial aluminosilicate fiber, and additionally having high compression recovery, or resiliency.

Upon heating to service temperature, the glass fibers, which are generally amorphous as manufactured, undergo crystallization. In part, the size of the resulting crystals affects the mechanical properties of the fiber. It has been observed that strong, resilient fibers demonstrate very small grain size after firing. Fibers which are fragile after firing typically have very large grains.

One measurement of after service grain size is conducted as follows. Fiber samples are fired at 1260°C (typically for 24 hours). The fired sample is then mounted in epoxy and the epoxy is allowed to harden. The epoxy mount is then polished to provide a smooth cross-section of the fiber. This polished mount is then examined using a scanning electron microscope operating in either the backscattered or secondary electron imaging mode (whichever gives the best contrast between the crystal phases) and a photomicrograph is taken.

A line is drawn across the micrograph (usually from corner to corner) and the number of crystal intersections with this line is counted. The length of the line is measured and converted to microns, based on the scale of

the photomicrograph. For example, a 5 cm line drawn on a 1000x micrograph would be measured as 5/1000 cm or 50 microns. The length of the line is divided by the number of crystal intersections to give an approximate size per crystal.

In some cases, crystal size is too small or boundaries too diffuse to allow measurement by this method. In such cases, the size of a "typical" crystal may be estimated by comparison to the micron bar on the micrograph.

We have found that the addition of zirconia to magnesium silicate fibers, in levels up to about 11 weight percent, improves the after-service microstructure and lowers the friability of the resulting non-durable, refractory glass fibers. We have found that this addition of zirconia in the fibers also results in the formation of very small scale microstructures when the fiber is exposed to temperatures of up to 1260°C for up to 24 hours. This small scale or fine microstructure provides good mechanical fiber integrity after exposure to the service temperature. This microstructure may coarsen slightly with prolonged exposure to use temperature; however, these fibers retain their improved mechanical properties after such extended exposure relative to other non-durable, temperature resistant fibers.

A mechanism by which small grain size may improve fiber strength is in creating a fiber with smaller irregularities, as a small grained fiber will have a smoother surface than a coarse-grained fiber. Surface flaws may act as stress raisers and provide points at which the fiber may be easily broken.

Although zirconia is known to decrease glass dissolution rates in SLF, in the fibers of the present

invention, this effect is shown to be sufficiently small so that the resulting fiber exhibits target solubility in SLF.

5 The combination of nondurability, that is, solubility
in SLF, and maintenance of mechanical integrity after
exposure to service temperatures of 1260°C, has not been
demonstrated by fibers disclosed or used by others in the
industry. The present invention controls fiber
10 microstructure upon devitrification, that is, heating to
service temperature, through the addition of up to 11
weight percent ZrO_2 , which modifies crystallization, to the
production melt.

15 Analysis of the durability of the above fibers in
simulated lung fluid indicates that these fibers are
significantly less durable than normal refractory ceramic
fiber, such as aluminosilicates (about 50/50 weight
percent) and alumino-zirconia-silicates or AZS (about
30/16/54 weight percent).

20 The non-durable refractory glass fibers according to
the present invention are made by standard glass and
ceramic fiber manufacturing methods. Raw materials, such
as silica, any suitable source of magnesia such as
25 enstatite, forsterite, magnesia, magnesite, calcined
magnesite, magnesium zirconate, periclase, steatite, or
talc, and any suitable source of zirconia such as
baddeleyite, magnesium zirconate, zircon or zirconia, are
delivered in selected proportions from bins to a furnace
30 where they are melted and blown using a fiberization
nozzle, or spun, either in a batch or a continuous mode.

35 The viscosity of the melt may optionally be controlled
by the presence of viscosity modifiers, sufficient to
provide the fiberization required for the desired
applications. The viscosity modifiers may be present in

the raw materials which supply the main components of the melt, or may, at least in part, be separately added. Desired particle size of the raw materials is determined by furnacing conditions, including furnace size (SEF), pour rate, melt temperature, residence time, and the like.

According to one embodiment of the present invention, the refractory glass fiber is capable of withstanding a use temperature of at least up to 1260°C with less than about 6% linear shrinkage, preferably less than about 4.5% linear shrinkage, exhibits low after service friability, and is non-durable in physiological fluids, such as lung fluid. Most preferably, the linear shrinkage of the fiber is less than about 3%. The non-durable refractory glass fiber of the present invention consists essentially of the product of about 65 to about 86 weight percent silica, about 14 to about 35 weight percent magnesia, 0 to about 11 weight percent zirconia, and optionally, an effective amount of a viscosity modifier. The fiber should contain not more than about 1 weight percent calcia impurity and not more than about 0.4 weight percent iron oxides impurity (calculated as Fe_2O_3). The viscosity modifier may be selected from alumina, boria and mixtures thereof. Other elements or compounds may be utilized as viscosity modifiers which, when added to the melt, affect the melt viscosity so as to approximate the profile, or shape, of the viscosity/temperature curve of a melt that is readily fiberizable, as discussed below.

Examples 1-2

The following compositions were tested to further assess the effect of zirconia on magnesium silicate composition performance. Samples having the nominal weight percent compositions set forth below were heat treated at 1260°C for up to 24 hours.

Table I

	SiO ₂ :	MgO:	ZrO ₂
Ex. 1	75	14	11
Ex. 2	75	19.5	5.5

5

These samples were examined and found to have good microstructures as required to provide good after-service mechanical strength.

10

Comparative Example A

Fiber having the nominal composition 71.5 wt% SiO₂, 24.5 wt% CaO, 3.2 wt% Al₂O₃, and 0.1 wt% TiO₂ was tested and was found to meet durability and shrinkage targets. This fiber failed, however, when heated rapidly. We have theorized that the failure of this sample was due to poor crystal nucleation in the fiber, and/or excessive alumina impurity.

15

Comparative Example B

Fiber having the composition 75.3 wt% SiO₂ and 21.0 wt% CaO, with 1.5 wt% TiO₂ added as a nucleating agent, was made which met durability and shrinkage targets, and was tolerant of rapid heating. However, this material had excessive after service friability, exhibiting poor resiliency and crumbling to the touch.

20

25

The samples were heat treated at 1260°C for 24 hours. Microstructural analysis by scanning electron microscopy revealed that titania-containing structures had a coarser microstructure.

30

Titania had a strong negative impact on the after-service integrity of calcium silicate fibers. At a level of 1.5 weight percent, titania caused substantial grain growth and very high after service friability (that is, low mechanical strength.) In contrast, the after-service

35

integrity of zirconia containing fibers was improved relative to titania containing fibers after short term heating (less than about one month).

5 Viscosity vs Temperature

 The shape of the viscosity vs. temperature curve for a glass composition is representative of the ease with which a melt will fiberize and thus, of the quality of the resulting fiber (affecting, for example, the fiber's shot
10 content, fiber diameter, and fiber length). Glasses generally have low viscosity at high temperatures. As temperature decreases, the viscosity increases. The value of the viscosity at a given temperature will vary as a function of composition, as will the overall steepness of
15 the viscosity vs. temperature curve.

 One approach to testing whether a fiber of a defined composition can be readily manufactured at an acceptable quality level is to determine whether the viscosity curve of the experimental chemistry matches that of a known
20 product which can be easily fiberized. Such a target viscosity curve is shown in Figure 1A, being the viscosity curve for a commercially-available spun aluminosilicate fiber, and in Figure 1B, being the viscosity curve for a commercially-available blown aluminosilicate fiber.

25 Figure 2 shows the viscosity curve for a magnesia-zirconia-silica fiber melt chemistry consisting of 75% SiO₂, 5.5% ZrO₂, and 19.5% MgO (by weight). The "noisy" area of the curve from 1800 - 1900°C is believed to be due
30 to phase separation or the onset of solidification. Figure 3 shows a similar curve for a 70% SiO₂, 5.5% ZrO₂, 24.5% MgO melt chemistry. Comparison of Figures 2 and 3 shows that dropping the SiO₂ level 5% results in a decrease in viscosity; however, neither curve approaches the target
35 viscosity curve of Figure 1A. Figure 4 shows the impact of adding 1 weight percent Al₂O₃ to the composition of Figure

2. The small addition of Al_2O_3 causes the viscosity curve to be displaced downward and shifts the phase separated region to lower temperatures. Although not shown here, a similar viscosity shift is observed with a small B_2O_3 addition (up to about 1 weight percent).

By adjusting both the SiO_2 and Al_2O_3 level of a magnesia-zirconia-silica chemistry, it was possible to obtain the viscosity curve shown in Figure 5 for a 72.3% SiO_2 , 5.4% ZrO_2 , 21.3% MgO , 1% Al_2O_3 by weight melt chemistry, which is nearly identical in shape between 1800°C and 2000°C (the effective spinning range) to the viscosity curve of the aluminosilicate spun chemistry shown in Figure 1A. At such low levels, Al_2O_3 and B_2O_3 additions have minimal effect on the fiber performance properties of the present invention, yet are effective in adjusting melt viscosity and improving fiber quality.

Figure 6 shows the viscosity curve for a magnesia-zirconia-silica fiber melt chemistry comprising 73.5% silica, 23% magnesia, and 3.5% zirconia, by weight. Figure 7 shows the viscosity curve for a magnesia-silica fiber melt chemistry comprising 73.5% silica and 26.5% magnesia, by weight. Both these curves approximate the target viscosity curve of Figure 1B for the commercially-available, blown aluminosilicate fiber. These fiber melt chemistries, according to the present invention, are well suited to fiberization by conventional blowing or spinning techniques.

Example 3

Non-durable refractory glass fibers according to the present invention having target shrinkage and mechanical strength characteristics for a service temperature of at least 1260°C are suitable to be fiberized from melts which

yield the compositions listed in Table II below.

Table II

	Composition	A	B	C
5	SiO ₂	72.3%	72.2%	72.2%
	MgO	21.3	21.2	21.2
	ZrO ₂	5.4	5.3	5.3
	Al ₂ O ₃	1.0	1.3	0.8
	B ₂ O ₃	---	---	0.5
10	CaO	< 1	< 1	< 1
	Fe ₂ O ₃	< 0.3	< 0.3	< 0.3

The non-durable refractory glass fiber, according to the invention, preferably consists essentially of the product of about 65 to about 86 weight percent silica, about 14 to about 35 weight percent magnesia, 0 to about 11 weight percent zirconia, 0 to about 3 weight percent alumina, and 0 to about 2 weight percent boria. Fiber having less than about 2 weight percent alumina exhibits superior properties.

In more preferred ranges, the non-durable refractory glass fiber consists essentially of the product of about 69 to about 80 weight percent silica, about 20 to about 31 weight percent magnesia, 0 to about 7 weight percent zirconia, 0 to about 2 weight percent alumina, and 0 to about 1 weight percent boria.

In most preferred ranges, the non-durable refractory glass fiber consists essentially of the product of about 70 to about 79 weight percent silica, about 20 to about 29 weight percent magnesia, about 1 to about 5 weight percent zirconia, 0 to about 1.5 weight percent alumina, and 0 to about 1 weight percent boria.

5 In the melt and fibers the present invention, the operable silica level is between about 65 and about 86 weight percent, with the upper level limited only by manufacturability. This is contrary to the teachings in the art, which state that fibers having silica levels above 70% are not manufacturable.

10 The fibers of the present invention preferably contain substantially no alkali metal, greater than trace impurities. The alkali metal content of these fibers is generally in the range of trace impurities, or hundredths of a percent at most, calculated as alkali metal oxide. Other impurities include calcia, in the amount of less than about 1 weight percent or as low as possible, and iron
15 oxides, in the amount of less than about 0.4 weight percent, calculated as Fe_2O_3 , or as low as possible.

20 In a series of test runs, the following refractory fiber compositions were produced by either spinning or blowing techniques, and tested for thermal performance at 1260°C and solubility in SLF. Individual compositions are listed in Table IIIA, and their thermal performances and solubility data are detailed below in Table IIIB.

TABLE III A

Ex.	MgO	ZrO ₂	SiO ₂	Al ₂ O ₃	CaO	Fe ₂ O ₃	B ₂ O ₃
4	18.7	4.87	73.0	1.19	0.70	0.21	
5	22.2	0.00	72.9	1.61	0.88	0.22	
6	21.4	0.95	73.7	1.71	0.81	0.21	
7	20.7	2.00	73.7	1.24	0.74	0.21	
8	20.1	3.42	73.2	1.37	0.70	0.20	0.5
9	21.2	5.3	72.2	0.8	<1	<0.3	
10	17.8	5.85	72.8	1.24	0.67	0.19	
11	17.5	6.87	72.3	1.23	0.63	0.19	
12	16.9	7.29	72.3	1.19	0.57	0.17	
Comp 13	16.8	34.1	46.4	0.97	0.77	0.35	
Comp 14	21.7	24.1	51.9	0.90	0.89	0.23	
Comp 15	25.5	16.9	55.7	0.76	0.77	0.24	
Comp 16	16.4	16.0	64.9	0.84	0.72	0.18	
Comp B	-Calcia-	-Titania-	-Silicate-	—	—	—	
Comp C	-Alumino-	-Zirconia-	-Silicate-	—	—	—	
Comp D	-Kaolin-	—	—	—	—	—	
Comp E	-Alumino-	-Silicate-	—	—	—	—	
17	15.6	11.50	70.1	0.65	0.54	0.18	
18	21	6.00	70.3	0.54	0.69	0.27	
19	20.9	5.78	70.7	0.25	0.68	0.24	
Comp 20	21.3	12.14	64.6	0.42	0.63	0.26	
21	24.9	5.78	66.8	0.23	0.79	0.27	
22	14.6	5.27	78.0	0.20	0.57	0.18	
23	11.9	10.50	75.8	0.29	0.52	0.17	
24	21.2	0.00	76.8	0.20	0.90	0.24	
25	20.8	5.7	71.7	1.19	0.28	0.34	
26	21.5	2.0	74.9	1.09	0.40	0.35	
27	21.4	3.4	73.2	1.02	0.38	0.27	
28	20.4	6.9	70.4	1.02	0.38	0.24	
29	19.7	5.5	72.2	0.3	0.67	0.35	0.9
30	20.2	5.5	71.6	0.3	0.30	0.24	0.8
31	20.6	5.4	71.8	1.13	0.46	0.37	
32	22.2	5.6	70.7	1.26	0.29	0.34	
33	22.8	5.5	70.1	0.56	0.22	0.36	
34	21.5	5.32	69.8	2.88	0.23	0.15	
35	19.6	5.4	72.6	1.8	0.36	0.25	
36	20.2	5.5	72.1	1.4	0.34	0.25	0.2
37	20.2	5.7	72.4	1.10	0.40	0.25	0.3
38	20.5	5.5	72.3	0.91	0.40	0.25	0.7
39	20.7	5.4	72.9	0.66	0.43	0.17	

TABLE III B

Example	Shrinkage (%) 1260°C/24Hrs	Shrinkage (%) 1260°C/168Hrs	Grain Size (Microns)	Compression Strength (psi)	Compressive Recovery (%)	Solubility (ng/cm ² -Hr)
4	4.3	4.8	1.2	12.8	10.6	60.4
5	4.1	5.2	1.3	16.2	5	327
6						
7	6.1	7.6		16.9	7.9	142
8						87.7
9				7.2	4.3	
10						
11	4.0	4.3		14.3	10.6	46.6
12	3.4	3.5	0.8	10.2	8.4	33.0
Comp 13	13.1	16.0		39	6.7	44.9
Comp 14	23.4			107.8	4.4	7.3
Comp 15	>25.0					93.4
Comp 16	8.2	7.2		17.2	8.7	9.7
Comp B			2.4	1.1	1.4	
Comp C			0.2	4.5	11.5	
Comp D			0.3	7.5	12.1	
Comp E				6.9	24.3	
17			1.9			32.9
18			1.6			76.8
19			1.2			87.8
Comp 20			3.5			24.7
21			1.2			84.9
22			1.0			98.6
23			0.8			33.3

III B Continued

Example	Shrinkage (%) 1260°C/24Hrs	Shrinkage (%) 1260°C/168Hrs	Grain Size (Microns)	Compression Strength (psi)	Compression Recovery (%)	Solubility (ng/cm ² -Hr) Too rapid to measure
24			0.7			
25	3.3			12.1	14.1	
26	5.7			16.3	11.2	
27	6.0			18.2	11.6	
28	3.8			16.4	15.5	
29	5.72			4	3	189
30	5.11			6.4	3.8	171
31	4.6			10.9	6.9	40.7
32	5.58			13.3	4.6	182
33	6.09			13.4	4.8	226
34	3.93			12.4	8	47
35	4.52			13.2	11.0	
36	4.58			16.8	13.8	
37	3.5			11.3	13.9	
38	3.9			11.5	9.1	
39	5.6			9.7	7	

Tests conducted on the zirconia-containing magnesium silicate fiber of Example 4 revealed that the fiber exhibited a shrinkage of only 4.3% after 24 hours at 1260°C, a dissolution rate of 60.4 ng/cm²-hr, and mechanical integrity which compares favorably to that of similarly treated, high mechanical strength conventional refractory ceramic fiber (Comparative Examples C, D and E). Other examples within the present invention demonstrating low shrinkage at use or service temperature include Examples 5-8, 10-12 and 25-39. Comparative Examples 13-16, with compositional ranges outside of the present invention demonstrate much higher shrinkage at service temperature.

We have identified particular non-durable refractory glass fibers, according to the present invention, which exhibit very low shrinkage, on the order of about 4.5% or lower after exposure to service temperature, and which have been manufactured from a melt having alumina as a viscosity modifier, having a composition within the range of about 69.75 to about 73.5 weight percent silica, about 16.75 to about 22.25 weight percent magnesia, 0 to about 7.5 weight percent zirconia, and about 1 to about 3 weight percent alumina.

We have further identified particular non-durable refractory glass fibers, according to the present invention, which exhibit very low shrinkage, on the order of about 4.5% or lower after exposure to service temperature, and which have been manufactured from a melt having alumina and boria as viscosity modifiers, having a composition within the range of about 71.5 to about 73.5 weight percent silica, about 19 to about 21.5 weight percent magnesia, about 5 to about 6 weight percent zirconia, and about 0.5 to about 2 weight percent alumina, and about 0.2 to about 1 weight percent boria.

The after-service microstructure of fibers prepared according to the present invention, as represented by Example 12 reported in Table III above, was tested for grain size according to the test procedure set forth above after exposure to a temperature of 1260°C. This was compared to the test results for the titania-containing calcium silicate fiber having the composition of Comparative Example B, above, and the refractory AZS (Comparative Example C) and kaolin (Comparative Example D) ceramic fibers.

The results of the tests are represented by the micrographs of Figures 8-13. The titania-calcium-silicate fiber of Comparative Example B (Figure 10), being extremely friable, exhibited significant surface roughness and large surface crystal grain size as compared to both the conventional refractory ceramic fibers of Comparative Examples C (Figure 8) and D (Figure 9), and Example 12, a fiber of the present invention (Figure 11) which exhibited a smoother surface and relatively smaller surface crystallites. Surface roughness and large surface crystals are undesirable, being associated with fiber friability and low mechanical strength.

The SLF-soluble fibers of the present invention, however, having significantly reduced after-service friability, exhibited very fine grained microstructure, having crystal grain sizes generally on the order of 1.9 microns or less as shown in Table III, Examples 4, 5, 12, 17-19, and 21-24. Comparative Example B, which is a titania-calcium-silicate fiber, and Comparative Example 20, which is a magnesia-zirconia-silicate outside the compositional range of the present invention, demonstrated a much larger grained after-service microstructure.

Figure 12 demonstrates in cross section the small-grained crystallites, both in absolute terms and with reference to the diameter of the fiber, present in a fiber of the present invention after exposure to a service
5 temperature of 1260°C for 24 hours. This high mechanical strength fiber is comparable in crystallite size to the very strong AZS fiber, shown in cross section in Figure 13, after exposure to a service temperature of 1426°C for 24 hours.

10

In a further series of test runs, the following refractory fiber compositions were produced by the blowing technique and tested for thermal performance at 1260°C and solubility in SLF. Individual compositions are listed in
15 Table IVA, and their thermal performances and solubility results are detailed below in Table IVB.

Table IV A

Example No.	Composition									
	SiO ₂	CaO	MgO	ZrO ₂	Al ₂ O ₃	F/l	DIAM.			
40	67.52	0.27	30.57	0.58	0.92	52	1.0			
41	70.07	0.30	23.07	5.97	0.48	25	1.6			
42	68.63	0.30	29.75	0.58	0.62	32	1.2			
43	73.87	0.15	19.05	6.03	0.84	26	5.1			
44	75.75	0.27	23.43	0.01	0.47	40	2.4			
45	75.62	0.27	23.58	0.01	0.43	35	3.6			
46	76.63	0.19	19.40	3.33	0.40	40	8.5			
47	67.53	0.25	30.26	0.01	1.86	40	1.4			
48	77.30	0.15	15.91	5.82	0.76	30	11.3			
49	76.08	0.28	23.16	0.01	0.40	43	3.6			
50	68.09	0.24	27.77	3.36	0.45	37	1.4			
51	72.67	0.18	23.20	3.46	0.41	46	2.0			
52	76.61	0.15	19.53	3.32	0.34	35	7.7			

F/l = Fiber Index

Table IV A Continued

Example No.	Composition	SiO ₂	CaO	MgO	ZrO ₂	Al ₂ O ₃	F/I	DIAM.
53		72.67	0.18	23.20	3.46	0.41	46	2.0
54		71.55	0.16	22.46	3.1	2.65	41	3.5
55		71.71	0.15	23.13	3.3	0.65	35	3.6
56		71.86	0.29	27.32	0.00	0.32	56	1.3
57		72.19	0.18	27.1	0	0.45	28	1.7
58		72.24	0.18	27.19	0	0.32	27	2.3
59		71.82	0.17	26.65	0	1.3	30	3.6

F/I = Fiber Index

Table IV B

Example No.	Shrink 1260°C/ 24hrs	Shrink 1260°C/ 168hrs	C.S. at 1260°C/ 24hrs	C.S. at 1260°C/ 168hrs	C.R. at 1260°C/ 24hrs	C.R. at 1260°C/ 168hrs	Delta Shrink	K
40	9.2	17.5	18.4		11.1		8.3	875+
41	7.3	10.3	17.3	18.5	10.0	5.2	3.0	100
42	2.0	14.2	6.9	22.3	17.3	4.5	12.2	826+
43	4.5	4.4	11.5	8.5	8.9	6.1	0.0	59
44	5.6	5.3	15.8	11.9	8.9	7.5	0.0	1450+
45	6.0	5.5	11.8	9.8	8.5	6.1	0.0	863
46	4.1	5.9	23.8	15.3	7.8	5.2	1.8	280
47	7.7	12.5	14.2	21.6	9.8	6.3	4.8	763+
48	5.3	6.2	11.5	8.5	9.9	4.8	0.9	54
49	4.3	4.0	10.9	6.8	6.4	6.8	0.0	1117
50	7.5	10.0	15.7	13.5	8.9	5.0	2.5	402
51	4.2	4.8	15.4	10.7	12.2	7.6	0.6	368
52	6.0	6.1	19.4	14.4	9.0	3.4	0.1	254

CS = Compression Strength (psi)

CR = Compression Recovery (%)

K = Solubility (ng/cm²/hr)

Table IV B Continued

Example No.	Shrinkage 1260°C/ 24hrs	Shrinkage 1260°C/ 168hrs	C.S. at 1260°C/ 24hrs	C.S. at 1260°C/ 168hrs	C.R. at 1260°C/ 24hrs	C.R. at 1260°C/ 168hrs	Delta Shrink	K
53	4.2	4.8	15.4	10.7	12.2	7.6	0.6	368
54	4.3	4.8	10.8	5.7	10.8	4.2	0.5	233
55	4.3	8	12.5	5.8	16.8	3.4	3.7	328
56	7.2	10.2	12.5	16.3	12.9	9.0	3.0	712 +
57	5.3	6.1	15.1	9.0	7.9	3.7	0.8	863
58	5.6	6.4	13	6.8	7.3	3.0	0.8	863
59	3.4	7.7	16.9	28.2	14.3	9.7	4.3	612

CS = Compression Strength (psi)

CR = Compression Recovery (%)

K = Solubility (ng/cm²/hr)

For the non-durable fibers according to the present invention, prepared by fiber blowing techniques, the best thermal performance results are exhibited by fibers blown from melt compositions containing about 70% silica and greater, having a fiber index of about 35 or greater, and a diameter of about two microns or greater. This performance is obtained with fiber diameters up to about 10 microns, although the only practical upper limit for fiber diameter according to the present invention is the ability to spin or blow product having the desired diameter.

Particularly preferred compositions for forming fibers from the melt include about 70 to about 77.5 weight percent silica, about 15.5 to about 30 weight percent magnesia, and 0 to about 6 weight percent zirconia. A suitable melt composition for forming fiber product is about 73.5 weight percent silica, about 23 to about 26.5 weight percent magnesia, 0 to about 3.5 weight percent zirconia, and impurities in the range of about 0.15 to about 0.3 weight percent calcia and about 0.32 to about 1.86 weight percent, generally about 0.32 to about 0.92 weight percent alumina. These fibers exhibit excellent shrinkage characteristics, as shown by the shrinkage data in Table IV B, including the Delta Shrink property, or the difference in shrinkage between one day and one week at the service temperature. The fibers also exhibit significant solubility in SLF, as demonstrated in Table IV B. Solubilities of 54 to over 1450 ng/cm²-hr were measured by the technique described above. (The "+" in the Table indicates an extremely rapid fiber dissolution rate which was not amenable to direct calculation. The value reported is the lower limit of the dissolution rate for the sample.)

The non-durable, low shrinkage, refractory glass fibers of the present invention compare favorably with conventional kaolin, AZS, and aluminosilicate durable

refractory ceramic fibers in terms of mechanical strength after exposure to service temperature. Fibers of the present invention generally tested in a range comparable to kaolin fibers for the 50% compression strength test and the compression recovery test. The fibers of the present invention exhibit significantly improved mechanical strength, measured as compression strength and compression recovery, compared to the titania-calcium-silicate fiber of Comparative Example B.

The refractory glass fiber according to the present invention, consisting essentially of magnesium silicate modified by the addition of particular percentages of zirconia and optionally, viscosity modifier additives, such as Al_2O_3 and B_2O_3 , and exhibiting fine grained microstructure after exposure to service temperatures of $1260^{\circ}C$, is up to 150 times more soluble in simulated lung fluid than standard refractory ceramic fiber and is capable of withstanding temperatures greater than $1000^{\circ}C$, up to $1260^{\circ}C$ with less than 6% linear shrinkage.

The SLF-soluble fibers of the present invention, exhibited significantly reduced after service friability, namely high mechanical strength, compared to the very stable SLF-durable aluminosilicate and alumino-zirconia-silicate fibers. The fibers of the present invention generally exhibit fine microstructure, and exhibit low friability and high mechanical strength, as well as low shrinkage upon exposure to the service temperature and high solubility in SLF.

The inventive fiber, therefore, retains the beneficial use characteristics of conventional refractory ceramic fiber, such as aluminosilicate fibers, namely undergoing limited shrinkage at high use temperatures. The inventive refractory glass fiber shrinks less than about 6% at a use

temperature of 1260°C, and retains good mechanical strength after service. The inventive fiber exhibits low after-service friability, exhibiting a small scale or fine grained microstructure after initial exposure to service temperature and high compression strength and compression recovery.

The inventive fiber may be manufactured with existing fiberization technology and formed into multiple products, including but not limited to needled blanket, paper, felt and bulk fiber. In addition to the advantages of conventional refractory ceramic fiber, the inventive fiber is 4 to 150 times more soluble in the simulated lung fluid, thus minimizing concerns over fiber inhalation.

Thus, the objects of the invention are accomplished by the present invention, which is not limited to the specific embodiments described above, but which includes variations modifications and equivalent embodiments defined by the following claims.

WE CLAIM:

- 1 1. A low shrinkage, refractory glass fiber having a use
2 temperature up to at least 1260°C, which maintains
3 mechanical integrity after exposure to the use temperature
4 and which is non-durable in physiological fluids,
5 consisting essentially of the product of about 65 to about
6 86 weight percent silica, about 14 to about 35 weight
7 percent magnesia, 0 to about 11 weight percent zirconia,
8 and optionally, an effective amount of a viscosity
9 modifier.
- 1 2. The fiber of claim 1 wherein the fiber consists
2 essentially of the product of about 69 to about 80 weight
3 percent silica, about 20 to about 31 weight percent
4 magnesia, 0 to about 7 weight percent zirconia, 0 to about
5 2 weight percent alumina, and 0 to about 1 weight percent
6 boria.
- 1 3. The fiber of claim 1 wherein the fiber consists
2 essentially of the product of about 70 to about 79 weight
3 percent silica, about 20 to about 29 weight percent
4 magnesia, about 1 to about 5 weight percent zirconia, 0 to
5 about 1.5 weight percent alumina, and 0 to about 1 weight
6 percent boria.
- 1 4. The fiber of claim 1, consisting essentially of the
2 product of about 70 to about 77.5 weight percent silica,
3 about 15.5 to about 30 weight percent magnesia, and 0 to
4 about 6 weight percent zirconia.
- 1 5. The fiber of any of claims 1 to 4 containing less than
2 about 1 weight percent of calcia impurity, less than about
3 0.4 weight percent of iron oxide impurity, calculated as
4 Fe₂O₃, and substantially no alkali metal oxide.

1 6. The fiber of claim 1 wherein zirconia is present in an
2 amount effective to limit after-service temperature grain
3 size.

1 7. The fiber of any of claims 1 to 6 exhibiting crystal
2 grain sizes of less than about 2 microns.

1 8. The fiber of any of claims 1 to 7 wherein said fiber
2 exhibits a shrinkage of less than about 4.5% at 1260°C.

1 9. The fiber of any of claims 1 to 8 wherein the fiber
2 exhibits a solubility of at least 30 ng/cm²-hr when exposed
3 as a 0.1g sample to a 0.3 ml/min flow of simulated lung
4 fluid at 37°C.

1 10. A process for the production of the low shrinkage
2 refractory glass fiber of any of claims 1 to 9 having a use
3 temperature up to at least 1260°C, which maintains
4 mechanical integrity after exposure to the use temperature
5 and which is non-durable in physiological fluids
6 comprising:
7 forming a melt with ingredients consisting essentially
8 of silica, magnesia, optionally zirconia, and optionally an
9 effective amount of a viscosity modifier, and
10 producing fibers from the melt.

1 11. The process of claim 10 including spinning the fibers
2 from the melt.

1 12. The process of claim 10 including blowing the fibers
2 from the melt.

1 / 11

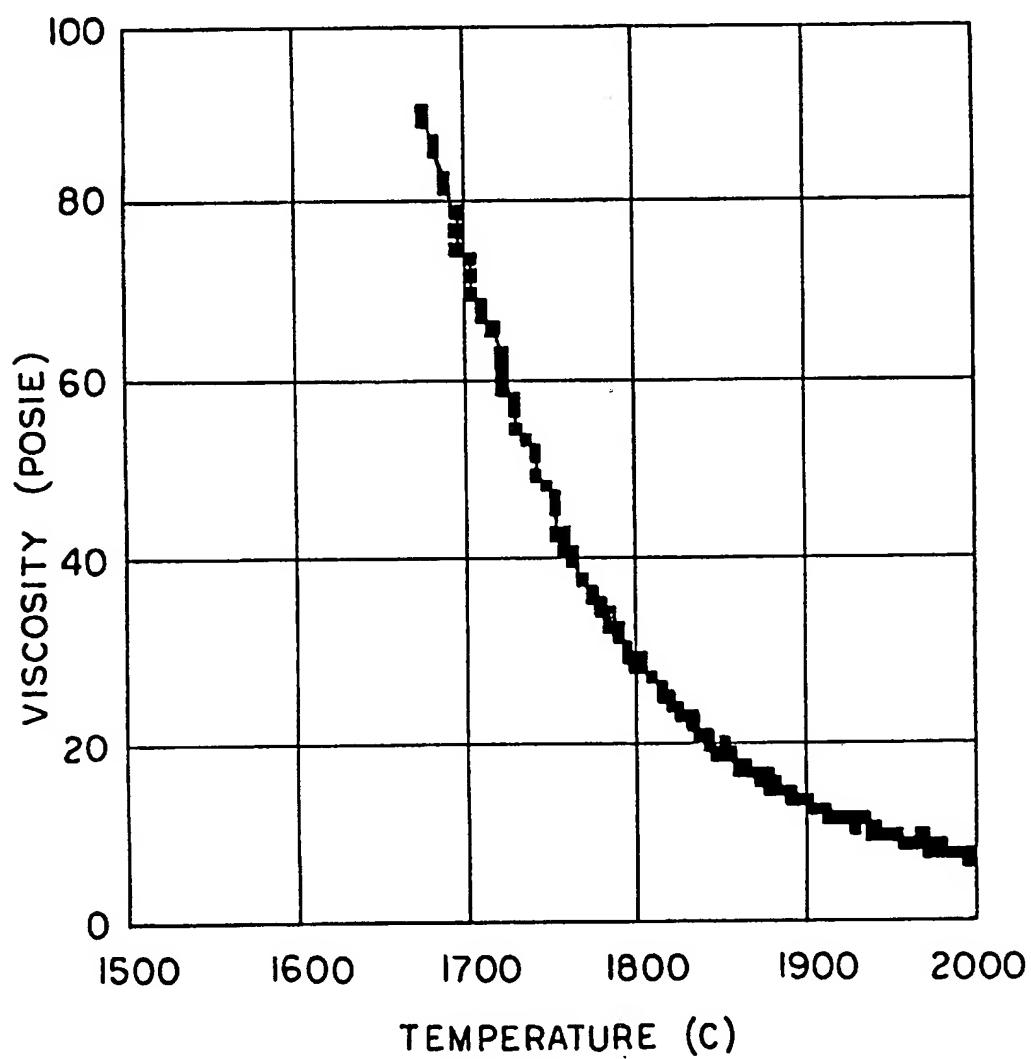


FIG. 1A

2/11

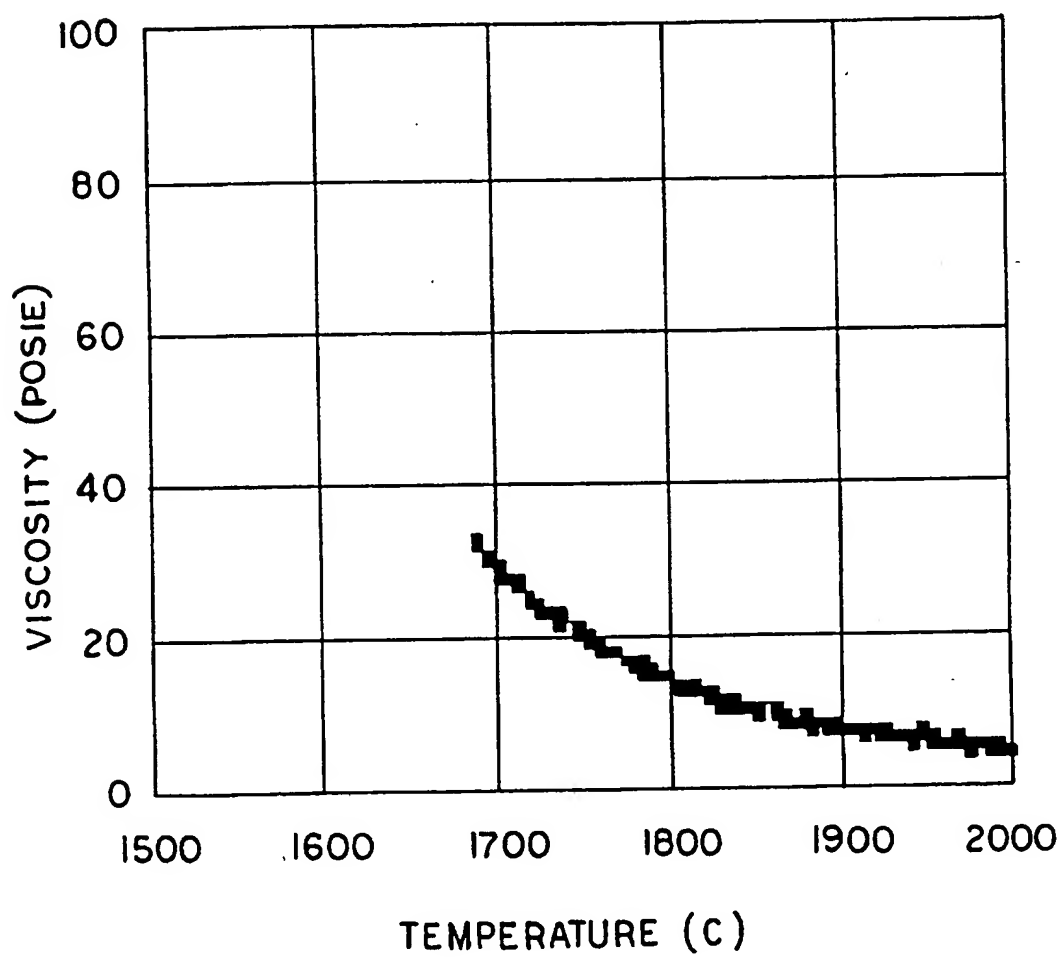


FIG. 1B

3/11

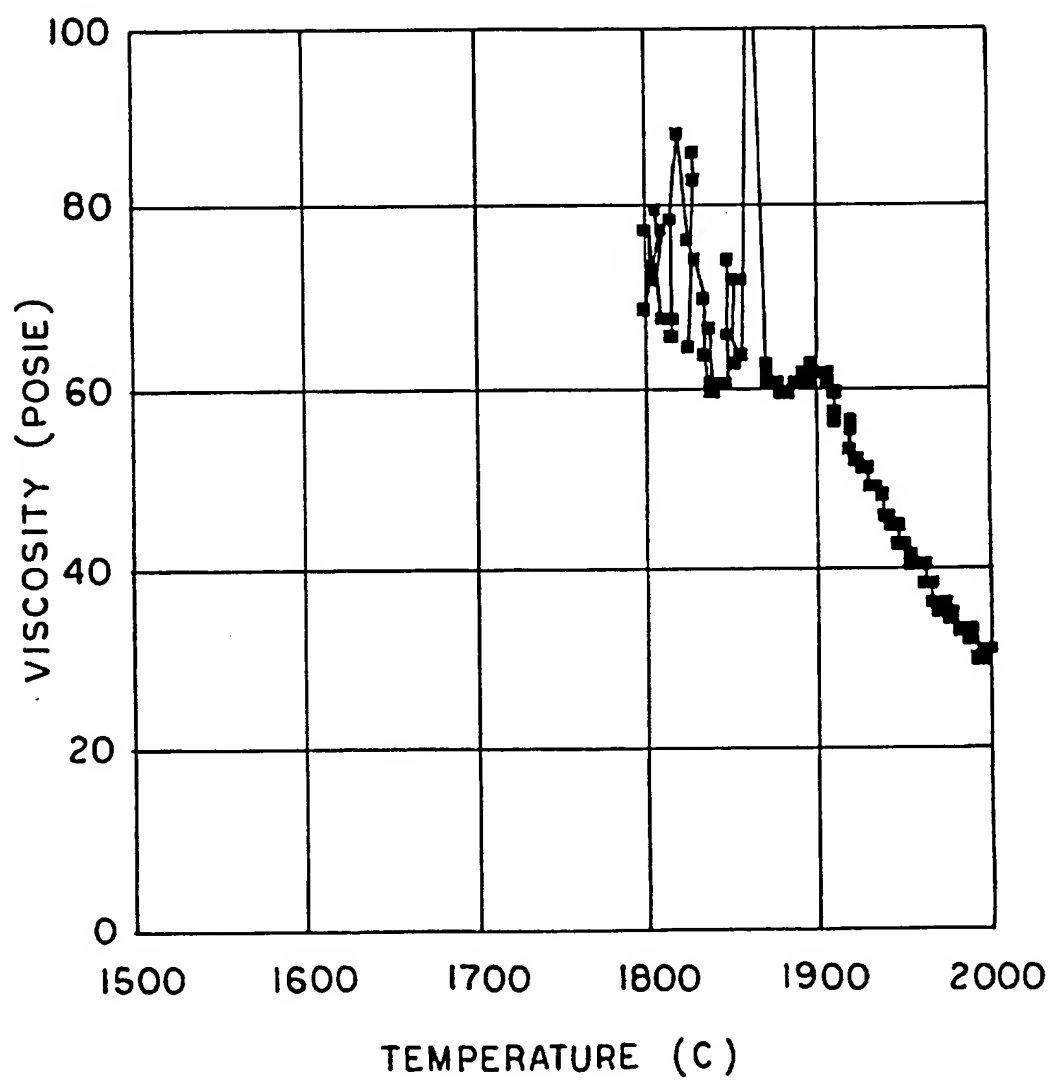


FIG. 2

4/11

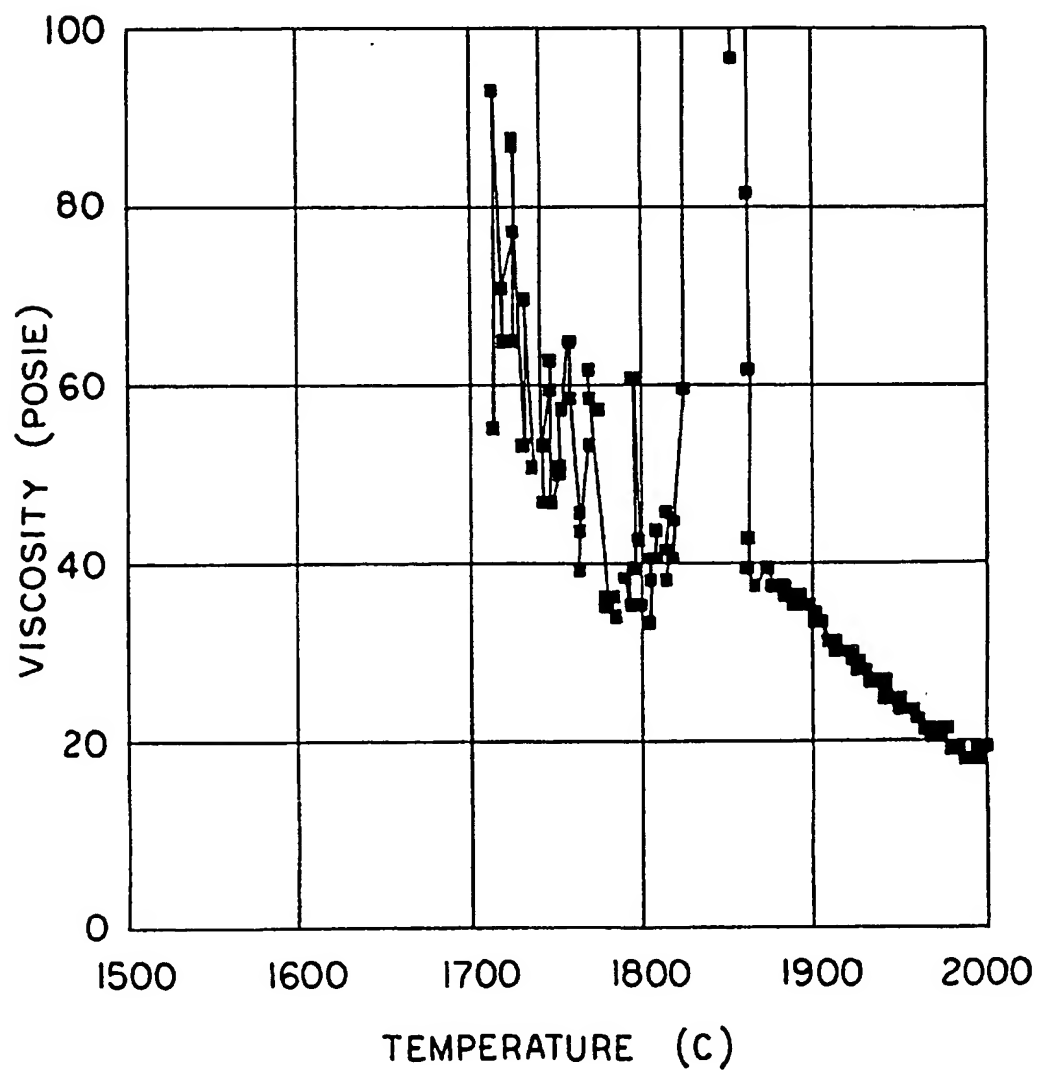


FIG. 3

5/11

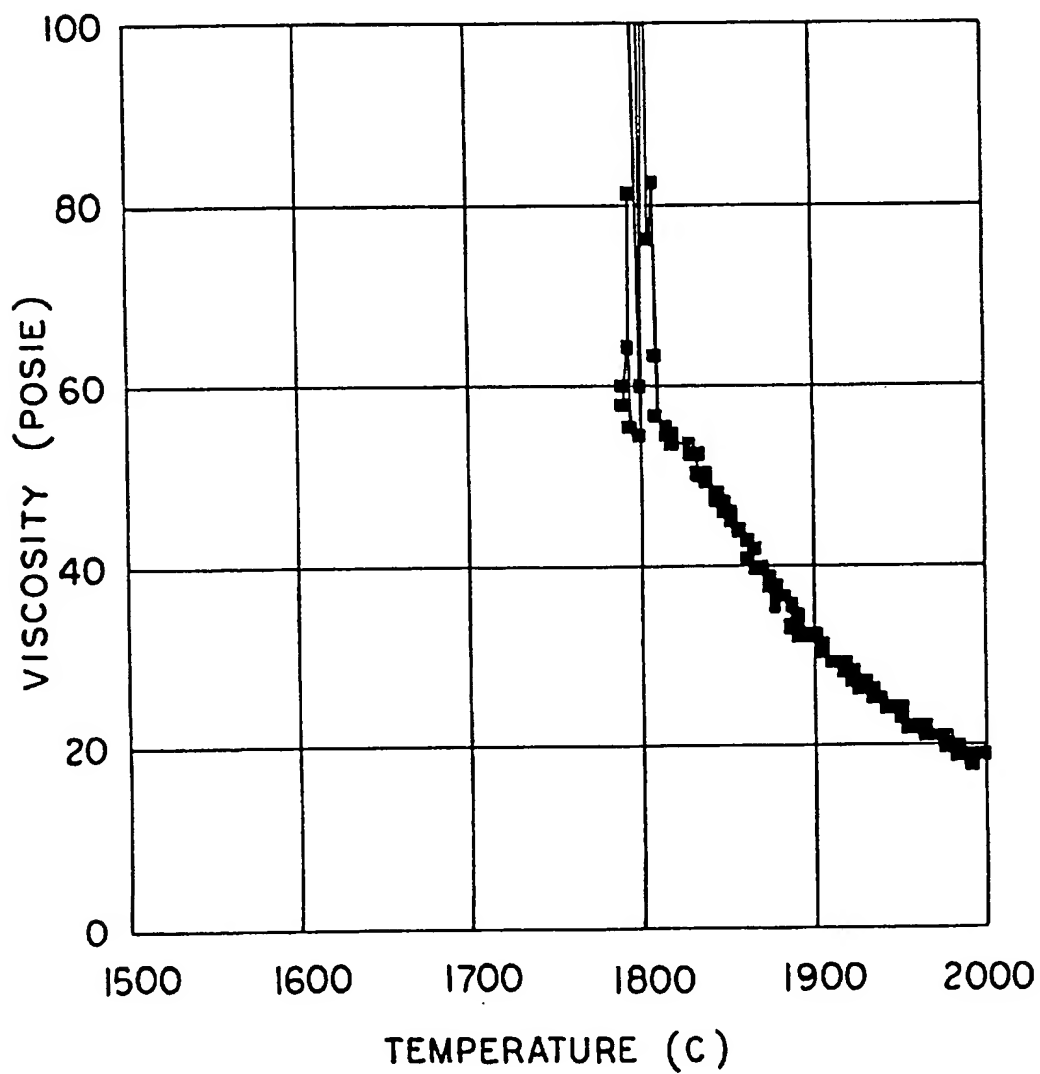


FIG. 4

6/11

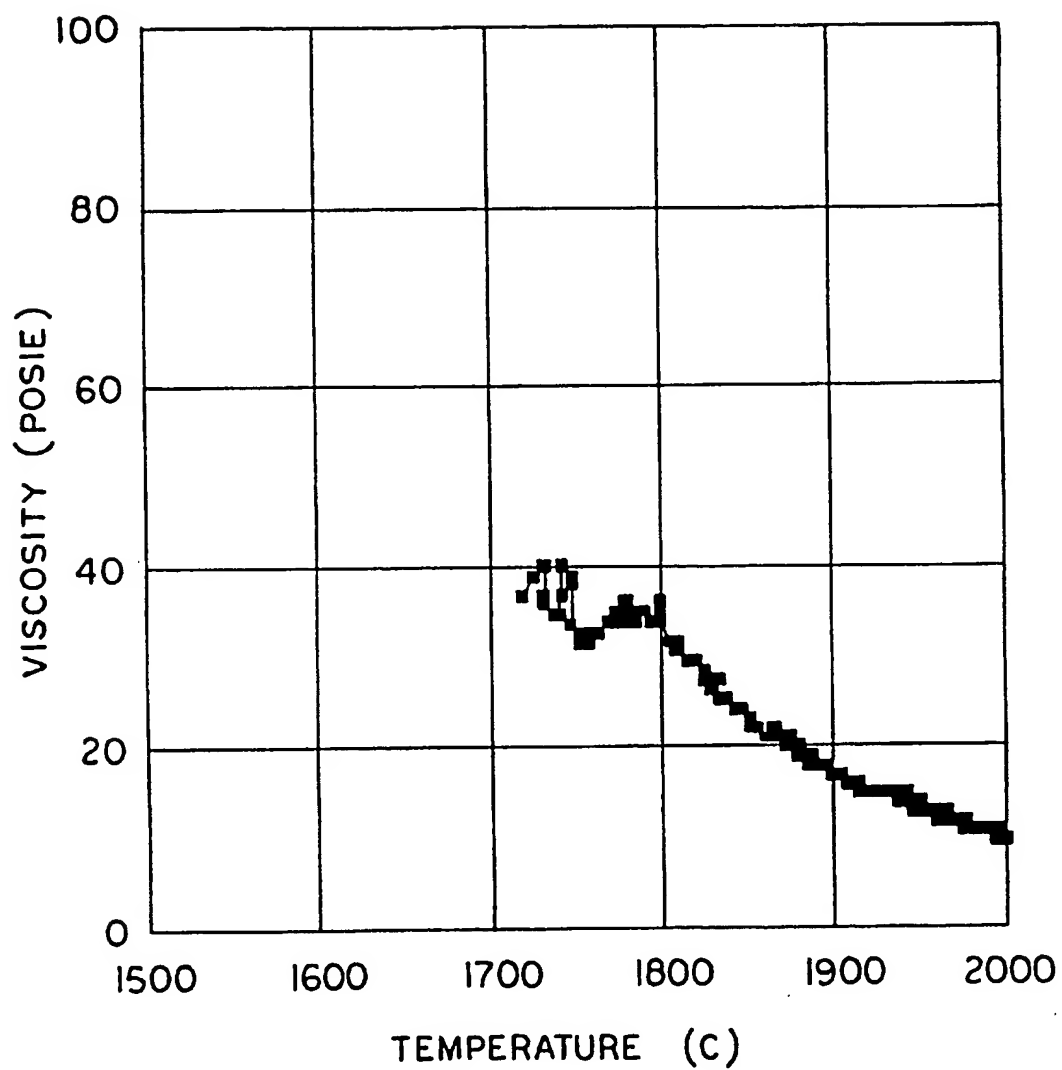


FIG. 5

7/11

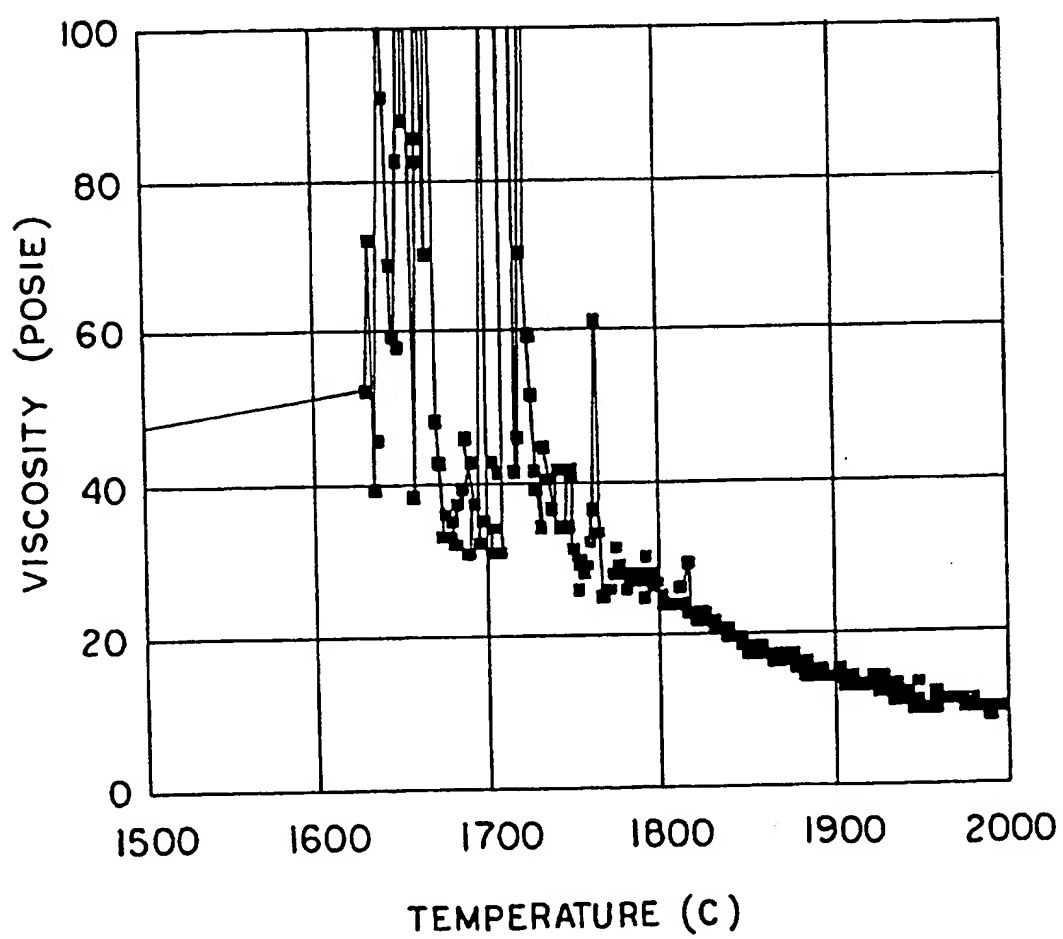


FIG. 6

8/11

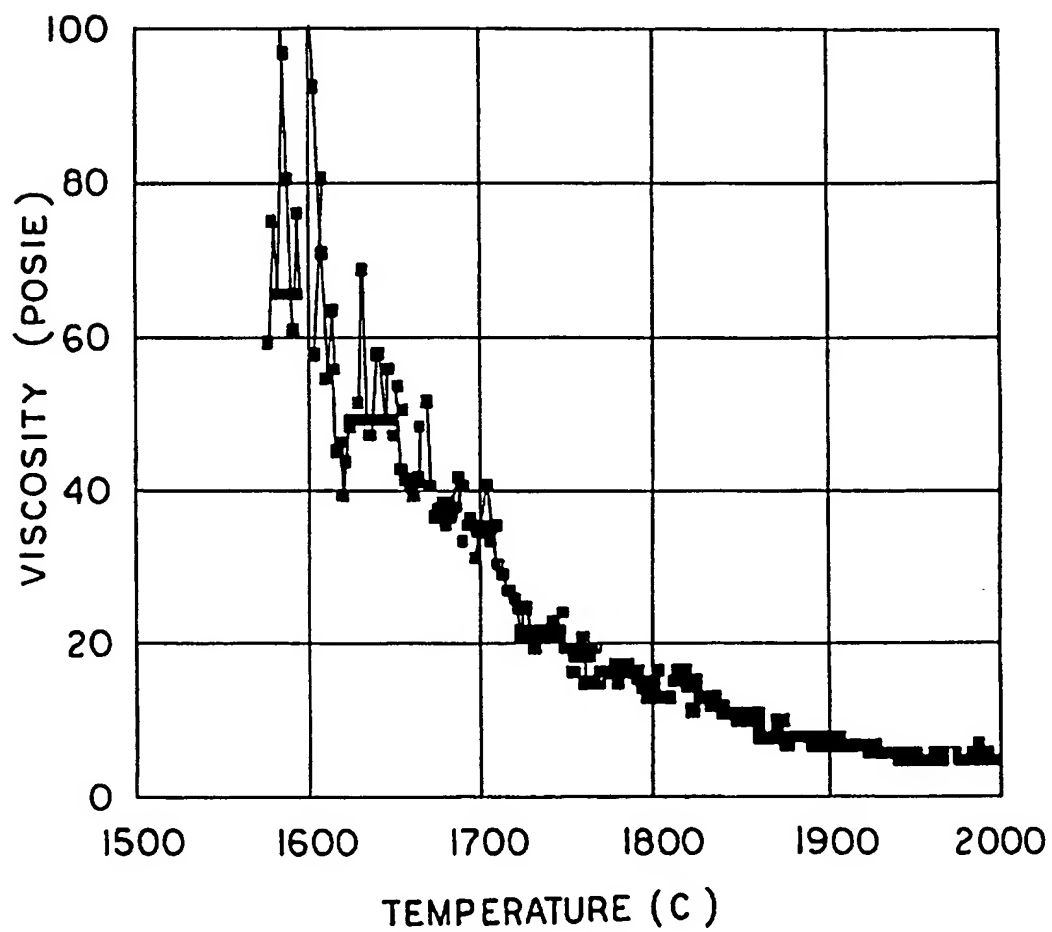


FIG. 7

9/11

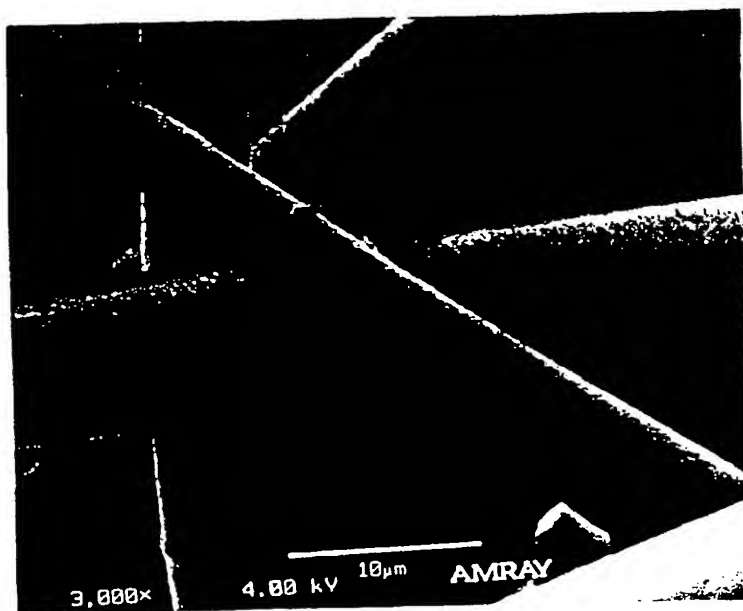


FIG.8

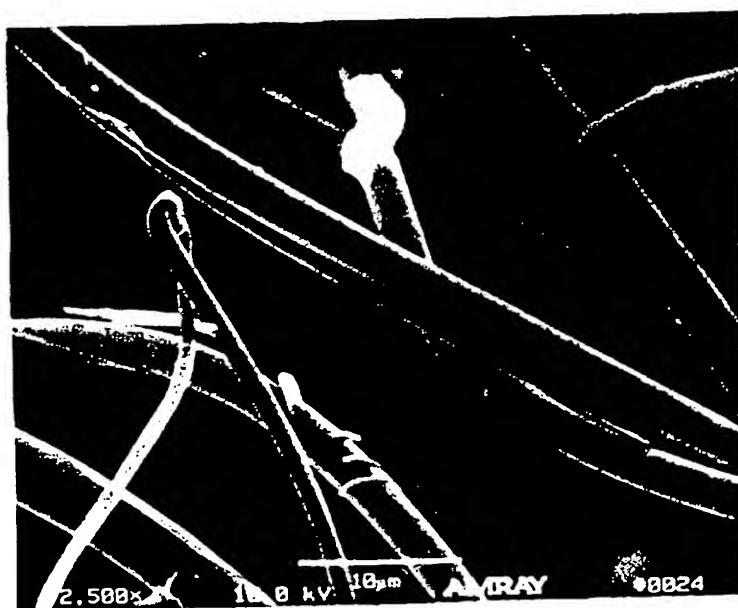


FIG.9

10/11

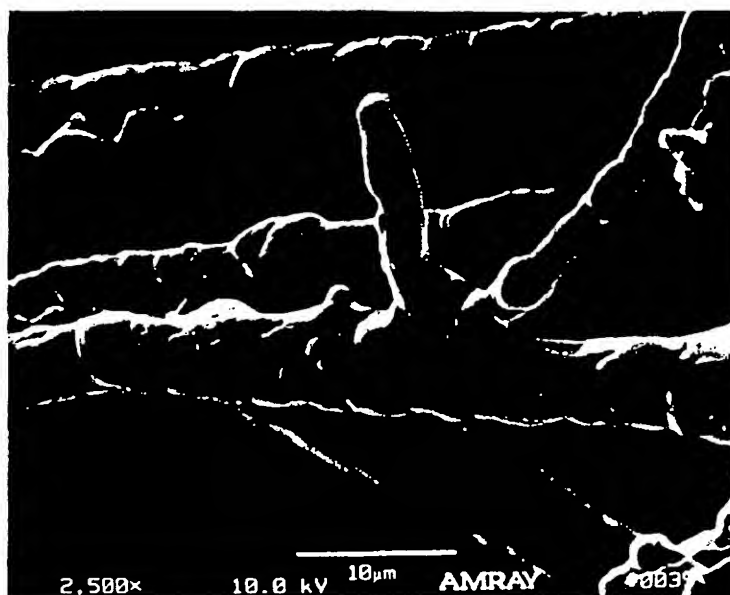


FIG. 10



FIG. 11

11/11

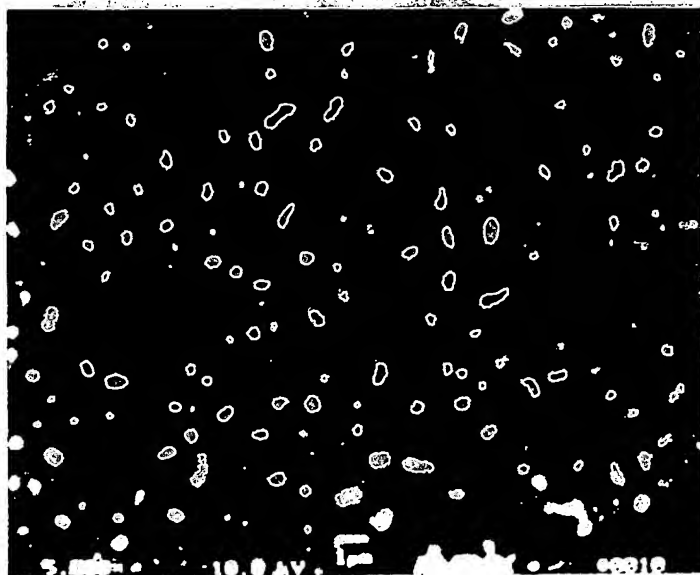


FIG.12

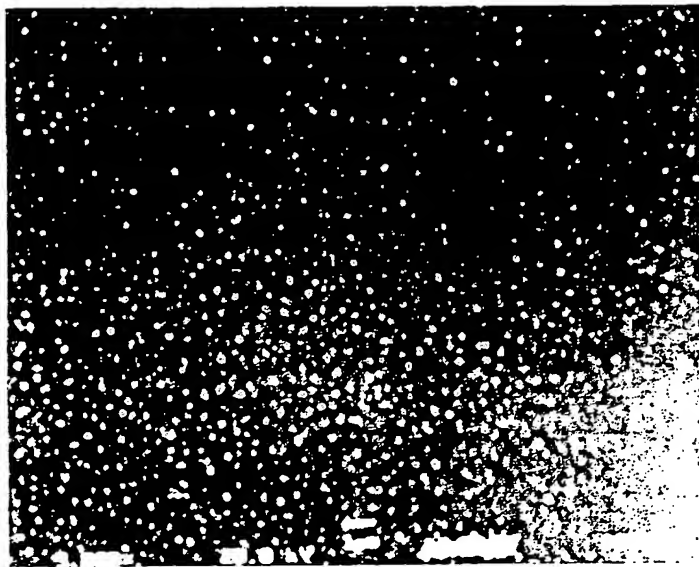


FIG.13

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US96/17494

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) : C03C 13/02

US CL : 501/38, 35, 72; 65/454, 475

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 501/38, 35, 72; 65/454, 475

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5,284,807 A (KOMORI ET AL) 8 February 1994, col. 3, lines 22-30, col. 12, lines 19-34.	1-12
Y	US 5,332,699 A (OLDS ET AL) 26 July 1994, col. 3, lines 5-39, col. 4, lines 23-41.	1-12
A	US 3,687,850 A (GAGIN) 29 August 1972.	
Y	US 5,569,629 A (TENECYCK ET AL) 29 October 1996, col. 2, lines 38-59.	1-12
Y,P	US 5,585,312 A (TENECYCK ET AL) 17 December 1996, col. 2, lines 35-59.	1-12



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents:	* T	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
* A* document defining the general state of the art which is not considered to be of particular relevance	* X	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
* E* earlier document published on or after the international filing date	* Y	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
* L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	* A*	document member of the same patent family
* O* document referring to an oral disclosure, use, exhibition or other means		
* P* document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search

14 JANUARY 1997

Date of mailing of the international search report

17 MAR 1997

Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. (703) 305-3599

Authorized officer

MARK BELL

Telephone No. (703) 308-3823